

# Cu<sub>2</sub>O-based catalysts for the electrochemical reduction of CO<sub>2</sub> at gas-diffusion electrodes

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## Abstract

Gas-diffusion electrodes are prepared with commercial Cu<sub>2</sub>O and Cu<sub>2</sub>O-ZnO mixtures deposited onto carbon papers and evaluated for the continuous CO<sub>2</sub> gas phase electroreduction in a filter-press electrochemical cell. The process mainly produced methanol, as well as ethanol and n-propanol. The analysis includes the evaluation of key variables with effect in the electroreduction process: current density ( $j$ = 10 to 40 mA·cm<sup>-2</sup>), electrolyte flow/area ratio ( $Q_e/A$ = 1 to 3 ml·min<sup>-1</sup>·cm<sup>-2</sup>) and CO<sub>2</sub> gas flow/area ratio ( $Q_g/A$ = 10 to 40 ml·min<sup>-1</sup>·cm<sup>-2</sup>), using a 0.5 M KHCO<sub>3</sub> aqueous solution.

The maximum CO<sub>2</sub> conversion efficiency to liquid-phase products was 54.8% and 31.4% for Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-based electrodes, at an applied potential of -1.39 and -1.16 V vs. Ag/AgCl, respectively. Besides, the Cu<sub>2</sub>O/ZnO electrodes are expected to catalyse the CO<sub>2</sub> electroreduction for over 20 h. These results may provide new insights into the development of powerful electrocatalysts for reduction of CO<sub>2</sub> in gas phase to alcohols.

**Keywords:** Electrochemical reduction, carbon dioxide, gas-diffusion electrode, copper oxide, methanol

## 1. Introduction

Carbon dioxide (CO<sub>2</sub>) concentration in the atmosphere is increasing each year by about 2 mg·l<sup>-1</sup>, continuing the inexorable rise toward 400 mg·l<sup>-1</sup> and beyond [1]. These high atmospheric CO<sub>2</sub> concentrations have been now widely accepted to produce severe environmental problems such as climate change. In the 21<sup>st</sup> century our world is still

searching for strategies to overcome the challenges associated with the climate change, as well as the dependency on fossil fuels and limited natural resources.

A variety of technologies to reduce CO<sub>2</sub> emissions have been applied through different methods. Currently, carbon capture and storage (CCS) has received considerable attention as one of the technologies to handle large quantities of CO<sub>2</sub> emissions [2], where CO<sub>2</sub> capture seems to be the bottleneck step where the efforts have to be applied [3-5]. Sequestration has been the major storage option for CO<sub>2</sub> gas from power plants, but several shortcomings remain, including environmental and safety concerns about the risk of leakage and technological limitations. Thus, new approaches to mitigate carbon output from the use of fossil fuels, as well as methods to fully exploit carbon neutral renewable energy sources are needed. A possible approach to slow down the increase in atmospheric CO<sub>2</sub> levels is the application of electrochemical methods in a Carbon Capture and Utilization (CCU) approach [6]. This technology is green and efficient and has aroused intense attention recently. The electrochemical reduction of CO<sub>2</sub> can not only offer a viable route to reuse CO<sub>2</sub>, but also a way to produce a number of valuable products, such as carbon monoxide (CO), formic acid (HCOOH), formaldehyde (CH<sub>2</sub>O), methanol (CH<sub>3</sub>OH), methane (CH<sub>4</sub>), ethanol (C<sub>2</sub>H<sub>6</sub>O), ethylene (C<sub>2</sub>H<sub>4</sub>) or n-propanol (C<sub>3</sub>H<sub>8</sub>O) [7-9]. Particularly, the challenges for converting CO<sub>2</sub> into CH<sub>3</sub>OH are great, but the potential rewards are also enormous [7, 10].

Currently, most electrodes used in the electroreduction of CO<sub>2</sub> are in the form of metal plates, metal granules or electrodeposited metals on a substrate [8]. However, owing to the relatively low solubility of CO<sub>2</sub> in water under ambient conditions, the reaction rates and current densities of CO<sub>2</sub> electroreduction are limited by the mass transfer of CO<sub>2</sub> from the bulk to the solid electrode surface [11, 12]. To improve the reduction process, gas diffusion electrodes (GDEs) have been proposed to alleviate mass transport limitations across the gas-liquid interface and to the catalyst surface [13-16]. A GDE is a porous composite electrode usually composed of polymer bonded catalyst particles and a carbon support. GDEs can be operated at higher current densities (200-600 mA·cm<sup>-2</sup>). Besides, because of their high porosity and partial hydrophobicity, GDEs form a characteristic gas-solid-liquid three-phase interface, which allows a homogeneous distribution over the catalyst surface. These properties make GDEs especially suitable for CO<sub>2</sub> electroreduction in gas phase.

While significant research efforts have focused on the development of new catalyst materials, considerably fewer efforts have focused on the study of these catalysts after immobilization in GDEs. In the same manner, the literature on the application of GDEs for the electrochemical transformation of CO<sub>2</sub> to CH<sub>3</sub>OH is scarce [17-20]. Schwartz et al. [17] firstly studied perovskite-type crystal structures (A<sub>1.8</sub>A'<sub>0.2</sub>CuO<sub>4</sub>, A = La, Pr and Gd; A' = Sr and Th) in GDE for the electrochemical reduction of CO<sub>2</sub> under ambient conditions. The results showed that perovskite-type electrocatalysts could achieve cumulative Faradaic efficiencies for CO<sub>2</sub> reduction to CH<sub>3</sub>OH, C<sub>2</sub>H<sub>6</sub>O, and C<sub>3</sub>H<sub>8</sub>O up to 40% at current densities of 180 mA·cm<sup>-2</sup>. In 2012, Aeshala et al. [18] developed Cu<sub>2</sub>O-based GDEs by electroplating the metal particles onto a carbon paper. These materials were settled in a reactor with different solid polymer electrolytes (i.e. SPEEK, Nafion, PVA, Amberlist) for continuous gas phase CO<sub>2</sub> electroreduction. The maximum Faradaic efficiencies were 0.54, 0.42, 0.3, and 4.5 for CH<sub>3</sub>OH, HCHO, CO and CH<sub>4</sub> production, respectively. The same group reported in 2013 a Faradaic efficiency as high as 45%, at a current density of 5.4 mA·cm<sup>-2</sup>, when applying an anionic solid polymer electrolyte membrane, with CH<sub>3</sub>OH as the main liquid product, and CH<sub>4</sub> and C<sub>2</sub>H<sub>4</sub> as major gaseous products. They concluded that the quaternary ammonium group in the solid polymer membrane, as well as the alleviated mass transfer limitation of CO<sub>2</sub> might have increase the efficiency of the GDE system [19]. Recently Lan et al. [20] investigated the electrochemical reduction of CO<sub>2</sub> on a Cu(core)/CuO(shell) catalyst in a flow reactor. This catalyst predominantly produce CO and HCOOH at 54.6 mA·cm<sup>-2</sup>, with a Faradaic efficiency of 21.5% and 20.2%, respectively. However, a small amount of CH<sub>3</sub>OH was also produced in the process (~2.5% Faradaic efficiency).

Furthermore, the literature demonstrated the good stability and notable catalytic ability of Cu<sub>2</sub>O-based surfaces for electrochemical hydrocarbons and/or alcohols formation from CO<sub>2</sub> [8, 11, 17-25]. Besides, the inclusion of ZnO may be the key for maintaining catalytic activity, since ZnO strengthen the Cu-CO<sup>-</sup> link, increasing the selectivity to alcohols, and stabilizing Cu in the hydrogenation reaction [11, 26-29]. Therefore, the primary objective of this study is to evaluate the performance of GDEs with spray supported Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO catalysts for the continuous electroreduction of CO<sub>2</sub> in gas phase. Then, an evaluation of the influence of key variables on the CO<sub>2</sub> electroreduction process (i.e. current density, electrolyte flow and CO<sub>2</sub> gas flow) is performed. The results are compared to those obtained in our previous work, where

mass transfer limitations were detected in the electroreduction of CO<sub>2</sub> in liquid phase when using a filter-press electrochemical cell.

The efforts carried out in this work will help to achieve the scale-up of CO<sub>2</sub> valorisation processes and devices in continuous operation, enabling a shift to a sustainable energy economy and chemical industry.

## **2. Materials and methods**

### *2.1. Preparation and characterization of the gas-diffusion electrodes*

The procedure to prepare the Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO GDEs has been described in detail previously [11]. The Cu<sub>2</sub>O-GDEs contain 1 mg·cm<sup>-2</sup> of metal particles. The catalyst loading was kept at 1 mg·cm<sup>-2</sup> of Cu<sub>2</sub>O and 1 mg·cm<sup>-2</sup> of ZnO for the Cu<sub>2</sub>O/ZnO electrodes. Briefly the procedure is as follows; Cu<sub>2</sub>O (Sigma Aldrich, particle size < 5 μm, 97% purity) and ZnO particles (ACROS organic, < 45 μm, 99.5%) were mixed with a Nafion<sup>®</sup> dispersion 5 wt.% (Alfa Aesar) and isopropanol (IPA) (Sigma Aldrich), with a 70/30 catalyst/Nafion mass ratio and a 3% solids (catalyst + Nafion). This ink was airbrushed onto a porous carbon paper (TGP-H-60, Toray Inc.) and dried to get the electrodes. All electrodes were dried and rinsed with deionised water before use.

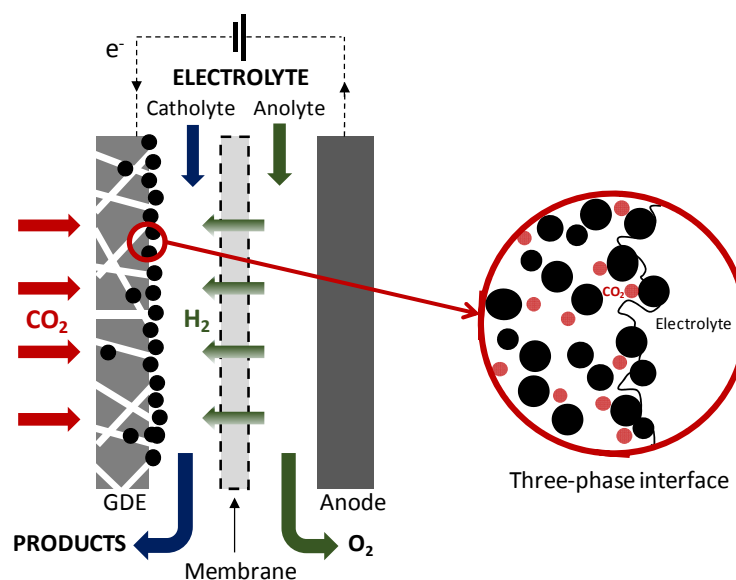
The EDX spectra and surface mapping confirmed the composition and uniform distribution of Cu<sub>2</sub>O-ZnO metal particles onto the carbon paper (See Figure A in Supporting Information). Thus, it can be inferred that the dispersion of the particles by air-brushing minimizes the agglomeration of the particles, which may greatly affect the electrode performance [23, 24, 29]. Besides the SEM cross-section image of the GDE shows that the diffusion layer (carbon paper) and the catalytic layer (Cu<sub>2</sub>O-ZnO) combined with each other tightly and the metallic particles covered nearly the entire carbon fibers of the support (See Figure B in Supporting Information).

### *2.2. Electrochemical cell and experimental conditions*

The components of the experimental setup have been described in detail elsewhere [13]. The electroreduction of CO<sub>2</sub> was carried out at ambient conditions using a filter-press electrochemical cell (Micro Flow Cell, ElectroCell A/S) in continuous operation. The cell was divided in a catholyte and anolyte compartments by a Nafion 117 cation exchange membrane. The membrane was treated prior the use following standard

procedures [30]. The airbrushed  $\text{Cu}_2\text{O}$  and  $\text{Cu}_2\text{O}/\text{ZnO}$ -catalysed papers were employed as the working electrodes (geometric area,  $A = 10 \text{ cm}^2$ ), together with a platinised titanium plate used as the counter electrode and a  $\text{Ag}/\text{AgCl}$  (sat.  $\text{KCl}$ ) reference electrode.

The cathode side of the reactor was fed with  $\text{CO}_2$  gas (99.99%) with a flow/area ratio ranging from 10 to  $40 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ , adjusted by a rotameter. A 0.5 M  $\text{KHCO}_3$  (Panreac) aqueous solution is used as both, catholyte and anolyte, with a flow rate ranging from 1 to  $3 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ . The electrolytes were pumped from catholyte and anolyte tanks to the cell by two peristaltic pumps (Watson Marlow 320, Watson Marlow Pumps Group). In this study, the filter-press electrochemical system possesses three inputs (catholyte, anolyte and  $\text{CO}_2$  separately) and two outputs (catholyte- $\text{CO}_2$  and anolyte) for the electroreduction of  $\text{CO}_2$  in gas phase. Figure 1 schematically represents the electrolytic GDE cell configuration for the electroreduction of  $\text{CO}_2$  supplied directly from the gas phase.



**Fig. 1.** Schematic diagram of the electrolytic cell configuration for the electroreduction of  $\text{CO}_2$  supplied directly from the gas phase

The experiments were performed at galvanostatic conditions (i.e. at a constant current density), using an AutoLab PGSTAT 302N potentiostat (Metrohm, Autolab B.V.). The current density ranged from  $j = 5$  to  $40 \text{ mA}\cdot\text{cm}^{-2}$  in the electrochemical experiments. Liquid samples were taken every 15 minutes from the catholyte tank with a total

operational time of 90 minutes, where pseudo-stable values are obtained [11]. All the experiments were carried out at ambient conditions.

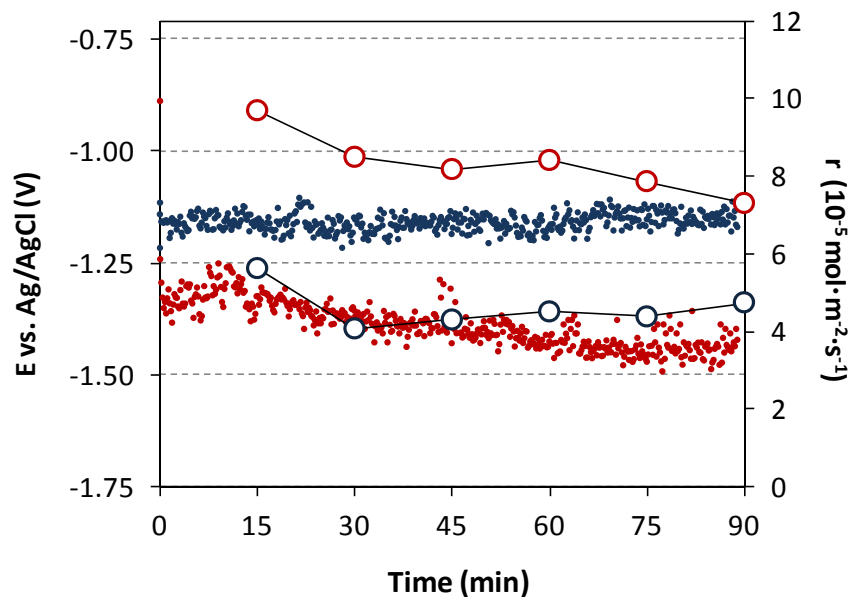
To quantify the concentration of each product in the liquid phase, the samples were analysed by duplicate in a headspace gas chromatograph (GCMS-QP2010, Ultra Shimadzu) equipped with a flame ionization detector (FID). Compounds were separated on a DB-Wax 30 m x 0.25 mm x 0.25  $\mu\text{m}$  column, with an injection and detector temperature of 250 °C and 270 °C, respectively. Helium was used as a carrier gas at a flow rate of 50  $\text{ml}\cdot\text{min}^{-1}$ . The identification of obtained products was further confirmed by headspace gas chromatography-mass spectrometry (GCMS-N5975B) using a 60 m x 250  $\mu\text{m}$  x 1.40  $\mu\text{m}$  DB-624 capillary column. Three replicates were performed for each sample to obtain an averaged concentration of the formed products. The standard deviations of all the experiments were below 18.6 %.

The performance of the electrochemical process is evaluated by the rate of product formation,  $r$  (i.e. product obtained per unit of cathode area and time), and the Faradaic efficiency,  $FE$  (i.e. selectivity of the reaction for the production of each product). The  $FE$  represents the percentage of the total charge supplied to the system that is used to form the different products.

### 3. Results and discussion

#### 3.1. Continuous electroreduction of $\text{CO}_2$ in a filter-press electrochemical cell

The electroreduction of  $\text{CO}_2$  at the  $\text{Cu}_2\text{O}$ -based GDEs led predominantly to the formation of  $\text{CH}_3\text{OH}$ , in accordance to those previous results at copper oxides surfaces [11, 24, 25]. Additionally, small quantities of  $\text{C}_2\text{H}_6\text{O}$  and  $\text{C}_3\text{H}_8\text{O}$  were also detected. Figure 2 shows the course of the applied voltage,  $E$ , and formation rate,  $r$ , of the main liquid-phase product,  $\text{CH}_3\text{OH}$ , over time for the  $\text{CO}_2$  electroreduction at both electrodes at ambient conditions.



**Fig. 2.** Electrocatalytic activity for the conversion of CO<sub>2</sub> at Cu<sub>2</sub>O (in red) and Cu<sub>2</sub>O/ZnO (in blue) GDEs. The figure shows the applied voltage,  $E$ , for a constant current of  $j=10\text{mA}\cdot\text{cm}^{-2}$  and the averaged rate of CH<sub>3</sub>OH formation,  $r$ , with time.

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171 From the figure, the required voltage,  $E$ , remains stable for the Cu<sub>2</sub>O/ZnO-based  
 172 electrodes over the course of the 90 minutes of operation. In contrast, the Cu<sub>2</sub>O  
 173 electrode required an increasing applied voltage to maintain a stable current ( $j=10$   
 174  $\text{mA}\cdot\text{cm}^{-2}$ ), which may be related to the progressive detachment of catalyst particles  
 175 from the GDE surface and the deactivation due to the exposure to concentrated CO<sub>2</sub> gas  
 176 [31, 32]. The observed fluctuations in required voltage can be explained as bubbles are  
 177 formed on the electrode surface, especially at Cu<sub>2</sub>O-based GDEs, where higher  
 178 potentials are required ( $E= -1.25$  to  $-1.50$  V vs. Ag/AgCl), in comparison to the  
 179 application of Cu<sub>2</sub>O/ZnO mixtures airbrushed onto the carbon papers ( $E= -1.16$  V vs.  
 180 Ag/AgCl). The lower potentials needed for Cu<sub>2</sub>O-ZnO mixtures are in agreement with  
 181 the higher cyclic voltammetry responses reported for Cu<sub>2</sub>O/ZnO-based electrodes in  
 182 comparison to those electrodes with deposited Cu<sub>2</sub>O particles, denoting the synergic  
 183 effect of Cu<sub>2</sub>O and ZnO in the current-potential reduction response [11].

184 Moreover, the rate of CH<sub>3</sub>OH formation,  $r$ , decreased for both electrodes as time went  
 185 on, and then stabilize uniquely for Cu<sub>2</sub>O/ZnO layers after 30 minutes of reaction at  $r=$   
 186  $\sim 4 \times 10^{-5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  until the end of the experiment. Probably, at the first experimental  
 187 minutes, the electrolyte penetrated into the internal structure of the GDE, enlarging the  
 188 contact area. This may explain the enhanced reaction rate at 15 min of operation,

indicating that the structure is sufficiently soaked and the three-phase liquid films had totally formed thoroughly the whole GDEs [33]. After this point, the GDE probably was to wet, limiting mass transfer to some extent and accumulating liquid-phase reaction products, which can partially block the electrode and reduce its electrochemically-active surface area [34-36]. Therefore, a gradual infiltration of electrolyte may be preferred for an enhanced CO<sub>2</sub> conversion at GDEs.

Table 1 shows the catalyst weight of the Cu-based samples after 30, 90 and 120 min of CO<sub>2</sub> electroreduction time. The total weight of catalyst placed in the carbon paper was 10 mg and 20 mg for Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-based electrodes, respectively.

**Table 1.** Particle loss for Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO GDEs before and after a CO<sub>2</sub> electroreduction period of 30, 90 and 120 min.

Electrode	Time (min)	Catalyst weight (mg)		Weight loss (%)
		Initial	Final	
Cu <sub>2</sub> O	30		9.04	9.56
	60	10	8.55	14.54
	90		7.97	20.35
Cu <sub>2</sub> O/ZnO	30		19.04	4.82
	60	20	18.72	6.41
	90		18.61	6.97

The results confirmed the more stable properties of Cu<sub>2</sub>O/ZnO surfaces in comparison to the Cu<sub>2</sub>O-based electrode, where the catalysts may be gradually peeled off from the carbon paper. Besides, defects in the catalytic layer would likely assist tunnelling and an increase the unwanted hydrogen formation due to easy access of water to catalytic sites. Therefore, a uniform and defect free catalyst layer is desired [16, 21]. According to the results, it is expected that Cu<sub>2</sub>O/ZnO layer could remain and catalyse the CO<sub>2</sub> electroreduction for over 20 h (if we consider the same particle detachment rate), since the total particle loss at 90 min was 1.39 mg of a total of 20 mg sprayed in the electrode. Overall, even if the Cu<sub>2</sub>O-based GDEs present an initial better performance for CH<sub>3</sub>OH formation, the utilization of Cu<sub>2</sub>O-ZnO mixtures is recommended for a continuous CO<sub>2</sub> electrochemical conversion due to its stable properties with time.



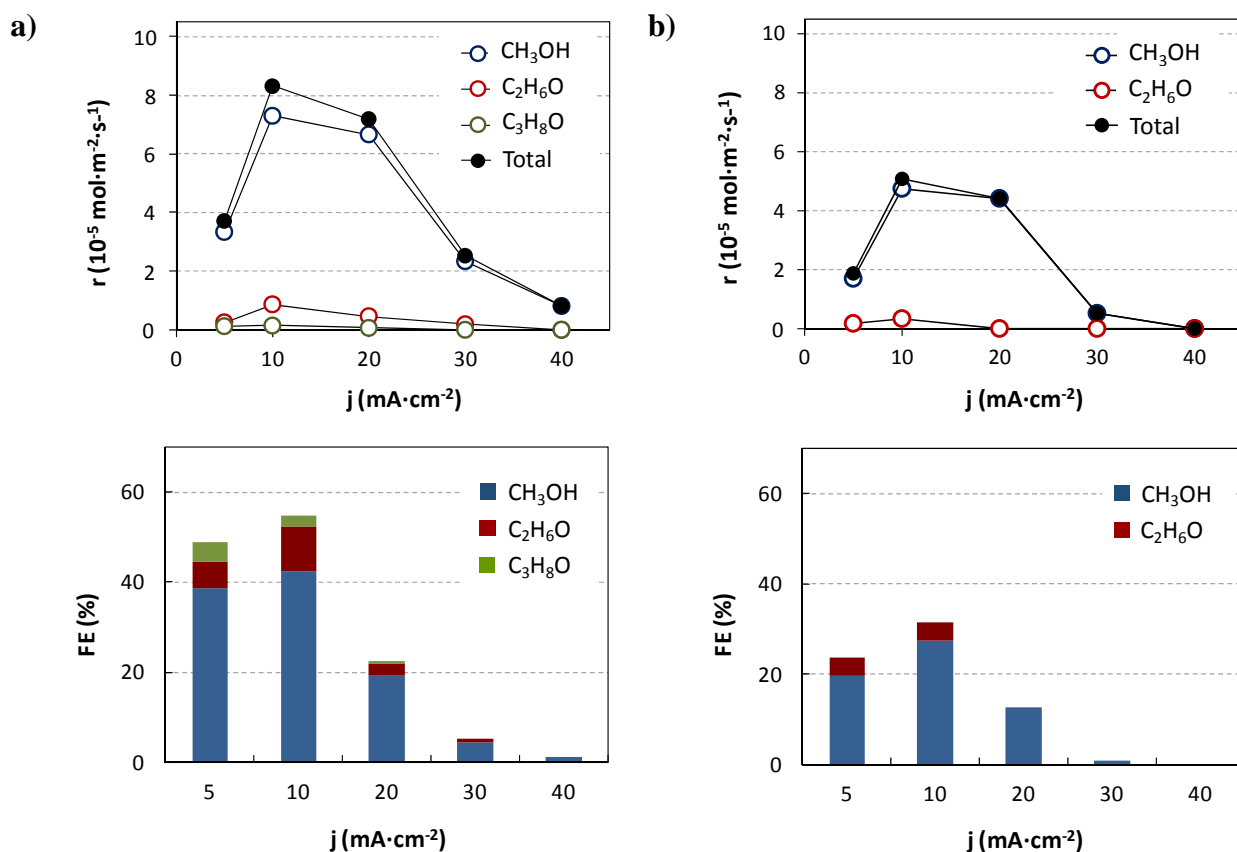
The averaged formation rate for Cu<sub>2</sub>O/ZnO surfaces at 90 min of operation takes the value of  $r = 4.74 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ , which is higher than that value reported in our previous work at Cu<sub>2</sub>O/ZnO particles deposited onto carbon papers (without the supply of CO<sub>2</sub> gas),  $r = 3.17 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  [11]. Besides, the stable formation rate obtained at Cu<sub>2</sub>O/ZnO-based electrode is in the range of those values previously reported for air-furnace oxidized Cu foils ( $r = 2.36 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ ) and electrochemical oxidized Cu foils ( $r = 2.78 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ ) at potentials ranging from -1.2 to -1.5 V vs. Ag/AgCl [21] or the CH<sub>3</sub>OH formation rates reached at electrodes based on Cu<sub>2</sub>O electrodeposited on stainless steel,  $r = 11.9 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  at -1.05 V vs. Ag/AgCl [25].

### 3.2. Key variables on the CO<sub>2</sub> electroreduction process

This section analyzes the influence of current density,  $j$ ; electrolyte flow/area ratio ( $Q_e/A$ ) and gas flow/area ratio ( $Q_g/A$ ) in the liquid-phase product distribution and the CO<sub>2</sub> conversion efficiency for the filter-press electrochemical system in continuous operation.

#### 3.2.1. Influence of current density

Figure 3 shows the quantitative information ( $r$  and  $FE$ ) regarding the liquid-phase product distribution at different current densities ( $j = 5$  to  $40 \text{ mA} \cdot \text{cm}^{-2}$ ).  $FE$  was calculated considering 6 electrons step pathways of CO<sub>2</sub> reduction to CH<sub>3</sub>OH, 12 electrons required per molecule of ethanol (C<sub>2</sub>H<sub>6</sub>O) and 18 to produce n-propanol (C<sub>3</sub>H<sub>8</sub>O). A constant electrolyte flow/area ratio ( $Q_e/A$ ) and gas flow/area ratio ( $Q_g/A$ ) of 2 and  $20 \text{ ml} \cdot \text{min}^{-1} \cdot \text{cm}^{-2}$ , respectively, were applied in the tests. It may be noted that the carbon paper without metallic particles supported did not produce any measurable liquid product.



**Fig. 3.** Rates of product formation,  $r$ , and Faraday efficiencies,  $FE$ , for the major products obtained from  $\text{CO}_2$  electroreduction at (a)  $\text{Cu}_2\text{O}$  and; (b)  $\text{Cu}_2\text{O}/\text{ZnO}$ -GDEs as a function of current density applied.

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239 The figures show that the product distribution and process efficiency is on dependence  
 240 of the current density applied. The system predominantly produces  $\text{CH}_3\text{OH}$ , with  
 241  $\text{C}_2\text{H}_6\text{O}$  as the second main product (which is a difficult reaction with 12 electrons  
 242 transfer required). The literature shows that the formation of  $\text{C}_2\text{H}_6\text{O}$  at Cu-based  
 243 electrodes is not unexpected [9, 37-42]. For example, Chi et al. [38] reported a good  
 244 selectivity for the formation of  $\text{C}_2\text{H}_6\text{O}$  ( $FE = 15.5\%$ ) for CuO nanoparticles deposited on  
 245 carbon papers when using a 0.2 M  $\text{KHCO}_3$  solution. Trace amounts of  $\text{CH}_3\text{OH}$  and  
 246  $\text{C}_3\text{H}_8\text{O}$  were also detected. Ren et al. [40] recently reported the formation of  $\text{C}_2$   
 247 compounds ( $\text{C}_2\text{H}_6\text{O}$  and  $\text{C}_2\text{H}_4$ ) on  $\text{Cu}_2\text{O}$  films at various electrochemical potentials. The  
 248  $FE$  was in the range of 9-16% for  $\text{C}_2\text{H}_6\text{O}$  formation in a 0.1 M  $\text{KHCO}_3$  electrolyte.  
 249 They hypothesized that  $\text{CO}_2$  is reduced through proton-electron transfer to give  $\text{HCOO}^-$   
 250 surface moiety, which can then hydrogenate to give  $\text{H}_2\text{O}$  and  $\text{CO}$  (adsorbed) at the  
 251 copper surface. These species can further hydrogenate to form  $\text{CH}_4$  or undergo  
 252 intermolecular C-C bond formation ( $\text{C}_1$  dimerization/hydrogenation) to yield  $\text{C}_2\text{H}_n\text{O}_2$   
 253 ( $n = 0-4$ ), which is further reduce to  $\text{C}_2\text{H}_6\text{O}$  and  $\text{C}_2\text{H}_4$ . The  $\text{Cu}^+$  ions were postulated to

be the catalytic active for reducing  $\text{CO}_2$  to  $\text{C}_2$  compounds. Besides, Li and co-workers demonstrated that  $\text{Cu}_2\text{O}$  films could reduce  $\text{CO}$  to  $\text{C}_2\text{H}_6\text{O}$  with a *FE* of 43% [41]. The metal particles boundaries on the surface (with undercoordinated Cu atoms) of the films were suggested to be the driving forces for  $\text{C}_1$  dimerization to form  $\text{C}_2$  products. Moreover, Kuhl et al. [9] evaluated the electrochemical reduction of  $\text{CO}_2$  on a Cu surface across a range of potentials and observed a total of 16 different  $\text{CO}_2$  reduction products (including  $\text{CH}_3\text{OH}$ ,  $\text{C}_2\text{H}_6\text{O}$  and  $\text{C}_3\text{H}_8\text{O}$ ). They discuss a scheme for the formation of multicarbon products and recognized that all the  $\text{C}_2$  and  $\text{C}_3$  products detected may have been produced via the dehydroxylation of an earlier, less reduced product in its enol or diol form. Therefore, they hypothesized that the chemistry to generate the wide range of multicarbon products may occur through an enol-like surface intermediate, that desorb to convert to its diol and/or keton form. The presence of hydroxyl and/or carbonyl moieties in many of the  $\text{C}_2$  and  $\text{C}_3$  products suggest that the C-C coupling step occurs before at least one of the two carbon-oxygen bonds in  $\text{CO}_2$  is broken. In any case, the mechanisms involved in C-C coupling reactions to form  $\text{C}_2$  and  $\text{C}_3$  products are still unclear. Certainly, further experimental work is needed to fully elucidate  $\text{CO}_2$  reduction steps on Cu surfaces.

The results also suggest that the reaction conditions created in the GDEs may be able to vary product selectivity if we compare the results with those obtained at identical catalytic materials but without  $\text{CO}_2$  supplied as gas, where  $\text{CH}_3\text{OH}$  was the main product, and only trace amounts of  $\text{C}_2\text{H}_6\text{O}$  were detected [11]. This is not exceptional if we consider those results obtained by Kas et al. for electrodes prepared with Cu nanoparticles for  $\text{CO}_2$  electroreduction to hydrocarbons [39, 42]. They proved that identical electrodes could yield predominately  $\text{CH}_4$  and  $\text{C}_2\text{H}_4$  depending on process conditions, such as the applied  $\text{CO}_2$  pressure, that can modify the conditions in the vicinity of the catalytic material. In theory, the GDE configuration changes  $\text{CO}_2$  transfer radically. Owing to the abundant pores in the GDEs,  $\text{CO}_2$  can diffuse to the electrode surface more conveniently than that from the bulk. Moreover,  $\text{CO}_2$  in the reaction can be obtained from  $\text{CO}_2$  (gas), rather than  $\text{CO}_2$  (aqueous) by use of GDEs, so that the concentration of  $\text{CO}_2$  (adsorbate) on the electrode surface can be increased [34] which probably may lead to the formation of more reduced species, altering the distribution of products from the reaction. It is also interesting to note the positive effects of supplying a  $\text{CO}_2$  gas flow through the electrode structure, which may provoke that the liquid

products diffuse more easily to the solution, avoiding the entrapment of liquid products into the carbon paper porous structure. Further research is required to fully understand this phenomenon.

Figure 3a and b reveal that the total rate of CO<sub>2</sub> reduction to liquid-phase products,  $r_T$ , did not improve at current densities higher than  $j = 10 \text{ mA}\cdot\text{cm}^{-2}$ , where a maximum value of  $r_T = 8.32 \times 10^{-5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  and  $r_T = 5.08 \times 10^{-5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  can be obtained at Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-based electrodes, respectively. In addition, the overall  $FE_T$  (the results of cumulative efficiencies for the formation of the different products) fell drastically as the current was increased from  $j = 10$  to  $40 \text{ mA}\cdot\text{cm}^{-2}$ . This may be explained as the additional current density applied is consumed by side reactions, such as the production of hydrogen (which competes with the electroreduction of CO<sub>2</sub> to useful products) and may indicate an optimal electrocatalytic current density of  $j = 10 \text{ mA}\cdot\text{cm}^{-2}$ , where the overall efficiency values can be as high as  $FE_T = 54.8\%$  and  $31.4\%$  for the Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-based surfaces, respectively.

Moreover, Table 2 compares the product distribution and  $FE$  for CO<sub>2</sub> conversion obtained in the present work with those previously obtained for the same materials in a CO<sub>2</sub>-saturated 0.5 M KHCO<sub>3</sub> solution (without CO<sub>2</sub> supplied as gas) [11]. The performance is, at the same time, compared with the values obtained in a CO<sub>2</sub>-saturated 0.5 M KHCO<sub>3</sub> solution when N<sub>2</sub> gas is supplied through the GDE structure (instead of CO<sub>2</sub>).

**Table 2.** Electrochemical reduction of CO<sub>2</sub> at Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO electrodes when CO<sub>2</sub> and N<sub>2</sub> gas flow through the GDE, and when no gas is supplied. Electrolyte flow/area ratio ( $Q_e/A$ ) =  $2 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ . Gas flow ratio ( $Q_g/A$ ) =  $20 \text{ ml}\cdot\text{min}^{-1}\cdot\text{cm}^{-2}$ .

Electrode	Flowing gas	$j \text{ (mA}\cdot\text{cm}^{-2})$	$E \text{ vs. Ag/AgCl}$	FE (%)			
				CH <sub>3</sub> OH	C <sub>2</sub> H <sub>6</sub> O	C <sub>3</sub> H <sub>8</sub> O	Total
Cu <sub>2</sub> O	CO <sub>2</sub>	10	1.39	42.3	10.1	2.4	54.8
	N <sub>2</sub>	10	1.52	40.2	2.3	-	42.5
	-	6.93 <sup>a</sup>	1.30	45.7	Trace	-	45.7
Cu <sub>2</sub> O/ZnO	CO <sub>2</sub>	10	1.16	27.5	3.9	-	31.4
	N <sub>2</sub>	10	1.69	18	1.5	-	19.5
	-	10.64 <sup>a</sup>	1.30	17.7	Trace	-	17.7

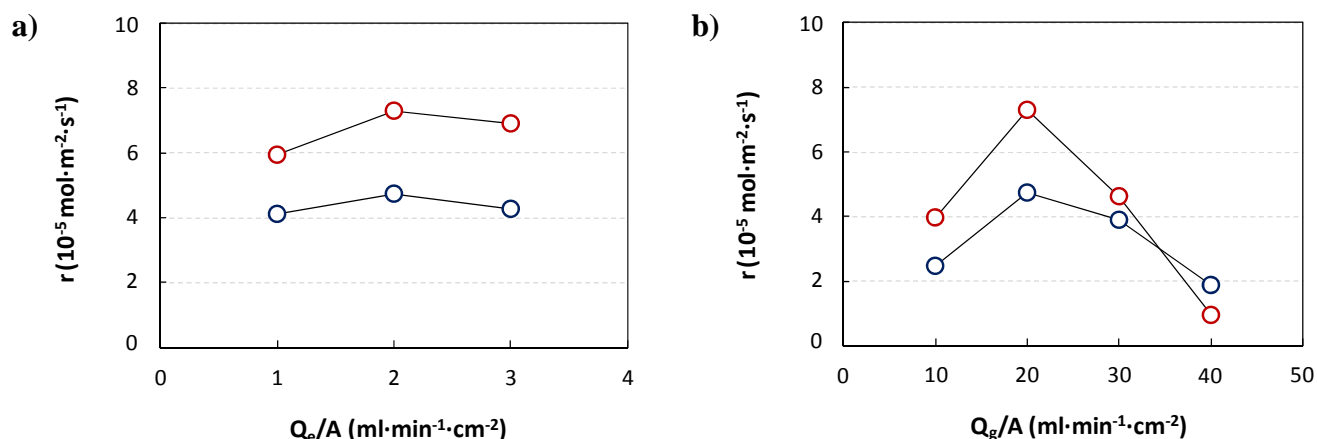
<sup>a</sup> Data from ref. [11]

The overall  $FE$  achieved for the conversion of  $CO_2$  demonstrated that the GDE with  $CO_2$  gas feeding to the electrocatalysts contributed to the high electrolysis efficiency, as compared to those results obtained at the identical electrodes when no  $CO_2$  as gas is supplied [11]. Besides, as observed from the results, the  $Cu_2O$ -GDE maintained a higher efficiency for  $CO_2$  reduction ( $FE_T= 54.8\%$ ) at higher current density ( $j=10\text{ mA}\cdot\text{cm}^{-2}$ ) than at  $Cu_2O$ -surfaces ( $FE_T= 45.7\%$ ) at lower current applied ( $j= 6.93\text{ mA}\cdot\text{cm}^{-2}$ ). This may indicate that the application of GDEs (with  $CO_2$  supplied as gas) is advantageous, since the process can be operated at higher current densities, while yielding higher  $CO_2$  reduction efficiencies.

Moreover, the efficiency values for the conversion of  $CO_2$  at GDEs are remarkably higher than those values obtained at a  $CO_2$ -saturated solution when  $N_2$  gas is supplied through the GDE structure, which suggest that the conversion of  $CO_2$  molecule can be not uniquely attributed to an enhanced agitation and diffusion of reactants in the electrochemical cell, but also to an increase of  $CO_2$  (adsorbate) available on the catalytic surface, leading to more reduced species.

### 3.2.2. Influence of electrolyte flow rate ( $Q_e/A$ ) and gas flow rate ( $Q_g/A$ )

In our previous study, external mass transfer limitations were detected in the filter-press electrochemical cell system [11], which might be overcome with the application of GDEs [13-16]. In order to improve the  $CO_2$  electroreduction performance, additional experiments were carried out at different electrolyte flow/area ratio ( $Q_e/A$ ) and  $CO_2$  gas flow/area ratio ( $Q_g/A$ ) and the results for the formation of the major product,  $CH_3OH$ , are presented in Figure 4a and b, respectively.



**Fig. 4.** Rate for CO<sub>2</sub> reduction to CH<sub>3</sub>OH,  $r$ , at (a) different electrolyte flow rate ( $Q_e/A$ ) and; (b) CO<sub>2</sub> gas flow rate ( $Q_g/A$ ) at the Cu<sub>2</sub>O (in red) and Cu<sub>2</sub>O/ZnO (in blue) GDEs. Current density:  $j = 10 \text{ mA} \cdot \text{cm}^{-2}$

335

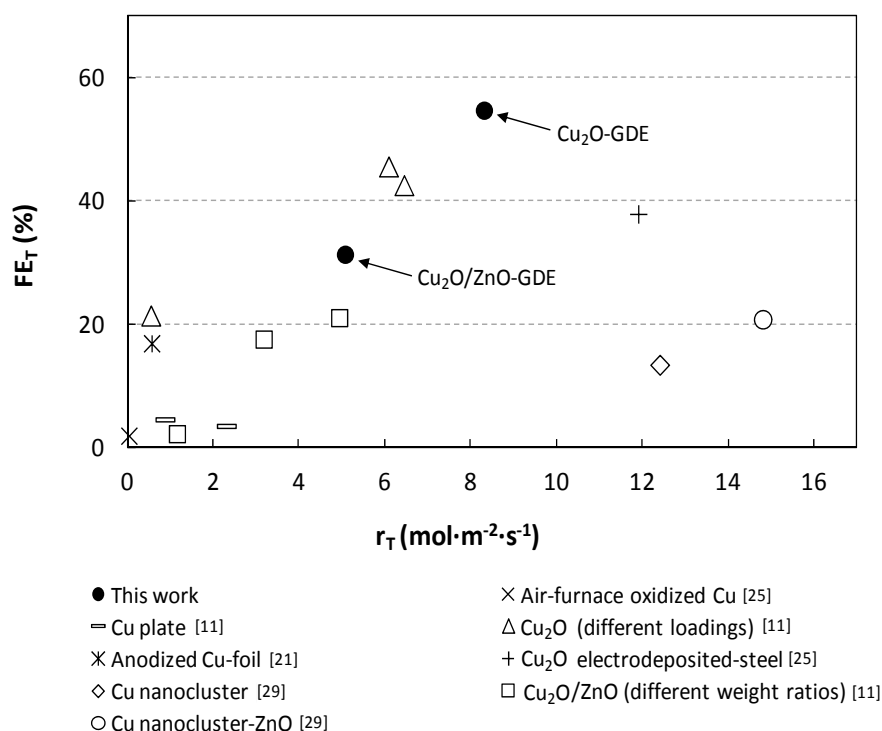
336 Firstly, Figure 4a shows that increases in  $Q_e/A$  from 1 to 3  $\text{ml} \cdot \text{min}^{-1}$  did not produce a  
 337 significant alteration in the rate of CO<sub>2</sub> electrochemical conversion to CH<sub>3</sub>OH, which  
 338 indicated that using low  $Q_e/A$  ratios is preferred in the GDE system since a more  
 339 concentrated product can be obtained without sacrificing the rate of CH<sub>3</sub>OH formation  
 340 (i.e. from 4.56 to 2.74  $\text{mg} \cdot \text{l}^{-1}$  at  $Q_e/A = 2$  and 3  $\text{ml} \cdot \text{min}^{-1}$ , respectively, at Cu<sub>2</sub>O/ZnO  
 341 GDE). Besides, lower electrolyte flows may allow a gradual infiltration of catholyte in  
 342 the GDE structure, which is preferred for an enhanced CO<sub>2</sub> electroreduction, as  
 343 discussed in section 3.1. Therefore, since process performance was only slightly  
 344 affected by the electrolyte flow, it can be concluded that the process may be primarily  
 345 limited by the internal diffusion of reactants through the porous structure of the GDE,  
 346 where the metal particles are deposited [13].

347 Additionally, Figure 4b demonstrated the importance of adjusts the optimal CO<sub>2</sub> gas  
 348 flow process. The lower formation rate ( $r = 2.48 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ ) for Cu<sub>2</sub>O/ZnO-based  
 349 electrode at  $Q_g/A = 10 \text{ ml} \cdot \text{min}^{-1} \cdot \text{cm}^{-2}$  in comparison to that value at  $Q_g/A = 20 \text{ ml} \cdot \text{min}^{-1} \cdot \text{cm}^{-2}$   
 350 ( $r = 4.74 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ ) indicated that the process is clearly limited by the  
 351 CO<sub>2</sub> gas supplied to the system. On the other hand, the application of a high CO<sub>2</sub> gas  
 352 flow of  $Q_g/A = 40 \text{ ml} \cdot \text{min}^{-1} \cdot \text{cm}^{-2}$  produced a severe decrease in the formation rate for  
 353 both electrodes, which can be partially attributed to the rapid detachment of metal  
 354 particles at these relatively high gas flows applied, in accordance with the main stability  
 355 limitations observed in GDE systems [15, 31, 43].

Therefore, the optimal point should provide enough CO<sub>2</sub> gas supply for the reaction, well before a massive detachment of metal particles occurs. This seems to happen at a flow range between  $Q_g/A = 20$  to  $30 \text{ ml} \cdot \text{min}^{-1} \cdot \text{cm}^{-2}$ . These results are interesting and should be taken into account in order to design efficient processes for CO<sub>2</sub> eletroreduction to CH<sub>3</sub>OH at GDE-based systems.

### 3.3. Comparison with other electrocatalytic materials

Finally, the results obtained in the present work for Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO-GDEs are compared with previous results for CO<sub>2</sub> electroreduction to liquid products at different Cu-based materials (when boht,  $r$  and  $FE$ , values available) at an applied potential range of  $E = -1$  to  $-1.5$  vs. V Ag/AgCl [11, 21, 25, 29]. Figure 5 represents the total rate of CO<sub>2</sub> conversion,  $r_T$ , vs. cumulative Faradaic efficiency,  $FE_T$ , reported in the literature for the formation of different liquid-phase products, including CH<sub>3</sub>OH. The figure uniquely provide a picture for comparison of CO<sub>2</sub> electroreduction performance, although other variables such as reaction medium, operating conditions and/or cell/electrode structure were applied, which may affect the results. The extraordinary high FE (i.e. >100%), where obviously both chemical and electrochemical steps involved in the CO<sub>2</sub> reduction process, obtained at anodized Cu foils and pre-oxidized Cu-TiO<sub>x</sub> electrodes [21] have been not included in order to clarify the analysis.



**Fig. 5.** Total rate of CO<sub>2</sub> conversion to liquid-phase products,  $r_T$ , vs. Faradaic efficiency,  $FE_T$ , for different Cu-based materials at E= -1 to -1.5 V vs. Ag/AgCl

As can be seen from the figure, the total CO<sub>2</sub> conversion efficiency obtained for GDEs in the present work outperformed those values observed at Cu, oxidized Cu and Cu-Zn surfaces, which may denote the positive effect of using GDEs. Nevertheless, the rate of CO<sub>2</sub> reduction to useful products is still below those values reported for Cu<sub>2</sub>O electrodeposited-steel electrode,  $r_T = 11.9 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  at -1.05 V vs. Ag/AgCl [25] or those values for Cu nanoclusters-ZnO mixtures at -1.4 V, where high total formation rates,  $r_T = 12.4 - 14.8 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$ , were reached. In any case, the relatively high CO<sub>2</sub> conversion rate to liquid products,  $r_T = 5.08 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  and total Faradaic efficiency,  $FE_T = 31.4\%$ , as well as the stable behavior, suggest the use of Cu<sub>2</sub>O/ZnO-based GDEs for the continuous electrochemical reduction of CO<sub>2</sub> to useful products, where CH<sub>3</sub>OH is the predominant product.

Future research should probably include the development of new highly active catalysts, as well as a deeper study to understand the relationship between GDE morphology and effective gas-liquid separation, while facilitating transport of reactants and products. These progresses may lead in the near future to an economically-viable CO<sub>2</sub> electrochemical process in continuous operation.



#### 4. Conclusions

This work demonstrated that the electroreduction of CO<sub>2</sub> to liquid products can be effectively carried out in continuous in a filter-press electrochemical cell equipped with Cu<sub>2</sub>O-based gas-diffusion electrodes (GDEs). The GDE configuration allows breaking through the mass transfer limitations usually found in electroreduction systems, producing an enhanced CO<sub>2</sub> reduction performance. The study included the experimental evaluation of key variables (i.e. current density,  $j$ ; electrolyte flow/area ratio,  $Q_e/A$ ; and CO<sub>2</sub> gas flow rate/area ratio,  $Q_g/A$ ) for the electrochemical conversion of CO<sub>2</sub> at Cu<sub>2</sub>O and Cu<sub>2</sub>O/ZnO commercial particles deposited onto carbon papers in a 0.5 M KHCO<sub>3</sub> catholyte under ambient conditions.

The experimental results in the filter-press electrochemical cell revealed that Cu<sub>2</sub>O/ZnO-GDEs are expected to remain stable over 20 h, in contrast to Cu<sub>2</sub>O surfaces that suffered a strong deactivation with time. The analysis of the liquid catholyte demonstrated that methanol was formed predominantly, with small amounts of ethanol and n-propanol.

The overall formation rate for the formation of liquid-phase products did not improve at current densities higher than  $j = 10 \text{ mA} \cdot \text{cm}^{-2}$ , where a maximum value of  $r_T = 5.08 \times 10^{-5} \text{ mol} \cdot \text{m}^{-2} \cdot \text{s}^{-1}$  was obtained at Cu<sub>2</sub>O/ZnO-GDEs. In addition, the overall *FE* (the results of cumulative efficiencies for the formation of the different products) fell drastically as the current was increased from  $j = 10$  to  $40 \text{ mA} \cdot \text{cm}^{-2}$ . The process performance was not affected by electrolyte flow, suggesting that the process may be primarily limited by the internal diffusion of reactants through the porous structure of the GDE, where the metal particles are deposited. In addition, the results demonstrated the importance of adjusting the optimal CO<sub>2</sub> gas flow in the electrochemical cell in order to supply enough CO<sub>2</sub> to react before a rapid detachment of metal particles from the catalytic surface occurred. Thus, the maximum efficiency detected at Cu<sub>2</sub>O/ZnO surfaces was  $FE_T = 31.4\%$  (at  $j = 10 \text{ mA} \cdot \text{cm}^{-2}$ ,  $Q_e/A = 2 \text{ ml} \cdot \text{min}^{-1} \cdot \text{cm}^{-2}$  and  $Q_g/A = 20 \text{ ml} \cdot \text{min}^{-1} \cdot \text{cm}^{-2}$ ), which is a significantly higher value than those results previously reported in literature for Cu-based electrodes and show the potential of Cu<sub>2</sub>O/ZnO-GDEs for the effective electrochemical valorization of CO<sub>2</sub>.

Overall, the results presented in this work are promising, but research efforts must be continued in order to develop new electroreduction systems based on highly active,

selective and stable materials to overcome the current limitations of the process before practical applications.

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